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**GATE 2024 Chemical Engineering (CH) Question Paper** 

**Graduate Aptitude Test in Engineering (GATE)**

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## **General Aptitude (GA)**

### **Q.1 – Q.5 Carry ONE mark Each**













#### **Q.6 – Q.10 Carry TWO marks Each**





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#### **Q.11 – Q.35 Carry ONE mark Each**









Q.14 A homogeneous azeotropic distillation process separates an azeotropic AB binary feed using a heavy entrainer, *E*, as shown in the figure. The loss of *E* in the two product streams is negligible so that *E* circulates around the process in a closedcircuit. For a distillation column with fully specified feed(s), given operating pressure, a single distillate stream and a single bottoms stream, the steady-state degrees of freedom equals 2. For the process in the figure with a fully specified *AB*  feed stream and given column operating pressures, the steady-state degrees of freedom equals









Q.17 Consider the steady, uni-directional diffusion of a binary mixture of  $A$  and  $B$  across a vertical slab of dimensions  $0.2 \text{ m} \times 0.1 \text{ m} \times 0.02 \text{ m}$  as shown in the figure. The total molar concentration of A and B is constant at 100 mol m<sup>-3</sup>. The mole fraction of  $A$  on the left and right faces of the slab are maintained at 0.8 and 0.2, respectively. If the binary diffusion coefficient  $D_{AB} = 1 \times 10^{-5} \text{ m}^2 \text{ s}^{-1}$ , the molar flow rate of A in mol s<sup>-1</sup>, along the horizontal *x* direction is  $\mathcal{X}$  $0.20<sub>m</sub>$  $0.10<sub>m</sub>$  $0.02 \text{ m}$ (A)  $\big| 6 \times 10^{-4}$ (B)  $\big| 6 \times 10^{-6}$ (C)  $3 \times 10^{-6}$ (D)  $3 \times 10^{-4}$ 







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#### **Q.36 – Q.65 Carry TWO marks Each**



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Q.57 Ethylene obeys the truncated virial equation-of-state

$$
\frac{PV}{RT} = 1 + \frac{BP}{RT}
$$

where *P* is the pressure, *V* is the molar volume, *T* is the absolute temperature and *B* is the second virial coefficient. The universal gas constant  $R = 83.14$  bar cm<sup>3</sup> mol<sup>-1</sup>K<sup>-1</sup>. At 340 K, the slope of the compressibility factor vs. pressure curve is  $-3.538 \times 10^{-3}$  bar<sup>-1</sup>. Let  $G<sup>R</sup>$  denote the molar residual Gibbs free energy. At these conditions, the value of  $\left(\frac{\partial G^R}{\partial P}\right)_T$ , in cm<sup>3</sup> mol<sup>-1</sup>, rounded off to 1 decimal place, is

Q.58 A metallic spherical particle of density 7001 kg m<sup>-3</sup> and diameter 1 mm is settling steadily due to gravity in a stagnant gas of density 1 kg m<sup>-3</sup> and viscosity  $10^{-5}$  kg m<sup>-1</sup> s<sup>-1</sup>. Take  $g = 9.8$  m s<sup>-2</sup>. Assume that the settling occurs in the regime where the drag coefficient  $C<sub>D</sub>$  is independent of the Reynolds number, and equals 0.44. The terminal settling velocity of the particle, in m  $s^{-1}$ , rounded off to 2 decimal places, is











 $Q.63$  Consider the surge drum in the figure. Initially the system is at steady-state with a hold-up  $\bar{V} = 5$  m<sup>3</sup>, which is 50% of full tank capacity,  $V_{full}$ , and volumetric flow rates  $F_{in} = F_{out} = 1 \text{ m}^3 \text{ h}^{-1}$ . The high hold-up alarm limit  $V_{high} = 0.8 V_{full}$  while the low hold-up alarm limit  $V_{low} = 0.2 V_{full}$ . A proportional (P-only) controller manipulates the outflow to regulate the hold-up V as  $F_{out} = K_c(V - \overline{V}) + \overline{F}_{out}$ . At  $t = 0$ ,  $F_{in}$  increases as a step from 1 m<sup>3</sup> h<sup>-1</sup> to 2 m<sup>3</sup> h<sup>-1</sup>. Assume linear control valves and instantaneous valve dynamics. Let  $K_c^{min}$  be the minimum controller gain that ensures *V* never exceeds  $V_{high}$ . The value of  $K_c^{min}$ , in  $h^{-1}$ , rounded off to 2 decimal places, is \_\_\_\_\_\_\_\_\_



Q. 64 | A PD controller with transfer function  $G_c$  is used to stabilize an open-loop unstable process with transfer function  $G_p$ , where

$$
G_c = K_c \frac{\tau_D s + 1}{\left(\frac{\tau_D}{20}\right)s + 1}, G_p = \frac{1}{(s - 1)(10s + 1)}
$$

and time is in minutes. From the necessary conditions for closed-loop stability, the maximum feasible value of  $\tau<sub>D</sub>$ , in minutes, rounded off to 1 decimal place, is

Q.65 Consider a tray-column of diameter 120 cm. Each downcomer has a cross-sectional area of 575 cm<sup>2</sup>. For a tray, the percentage column cross-sectional area not available for vapour flow due to the downcomers, rounded off to 1 decimal place, is  $\overline{\phantom{a}}$